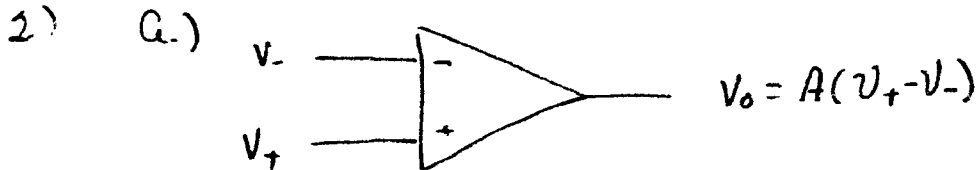


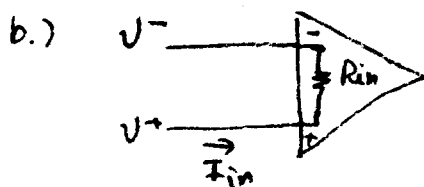
# Homework Set #5 Electronics

- 1.) Input resistance of amp:  $R_{in} \rightarrow \infty$   
 Amplification factor of amp:  $A \rightarrow \infty$



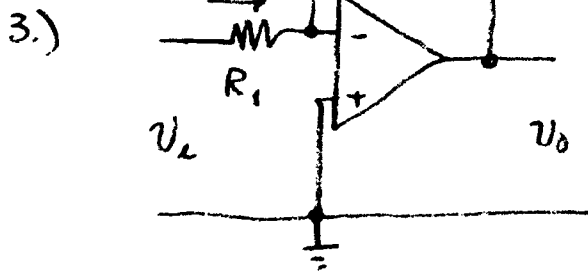
For  $V_o$  to be less than the limits set by the power supply,

$$(V_+ - V_-) < \frac{V_{limit}}{A} \quad \text{as } A \rightarrow \infty, \underline{V_+ - V_- \rightarrow 0}$$



$$I_{in} = \frac{V_+ - V_-}{R_{in}}$$

$$\lim_{R_{in} \rightarrow \infty} I_{in} = \lim_{R_{in} \rightarrow \infty} \left( \frac{V_+ - V_-}{R_{in}} \right) = 0$$



Since  $V^+ = 0$ , and  $V^- = V^+$ ,  
 $V^- = 0$ , thus

$$I = \frac{V_L - V^-}{R_1} = \frac{V_L}{R_1}$$

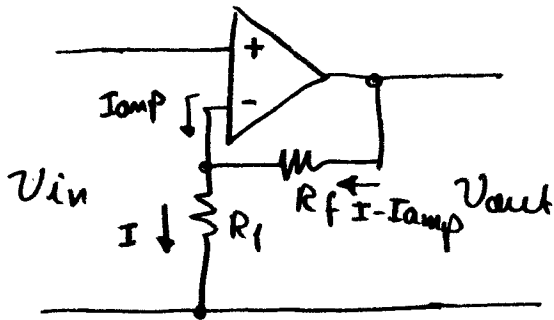
Since  $I_{amp} = 0$ ,  $I - I_{amp} = I$ .

$$V_o = -I R_f = -\frac{V_L R_f}{R_1}$$

$$G = \frac{V_o}{V_L} = -\frac{R_f}{R_1}$$

Set #5, cont

4.)

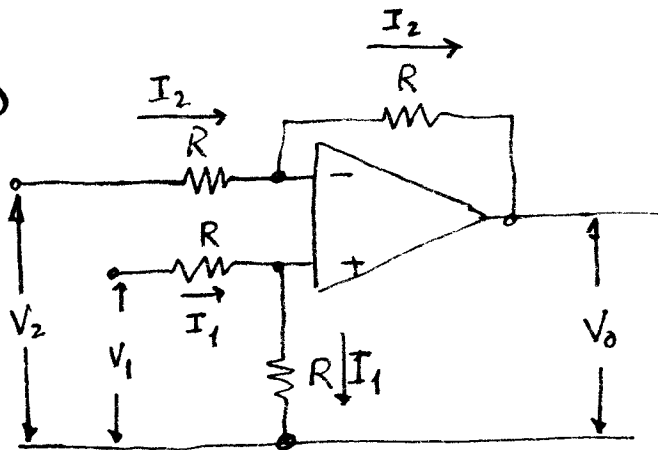


Since  $V_+ = V_{in}$ , and  
 $V_+ = V_-$ ,  $V_- = V_{in}$ ,  
 and  $I = \frac{V_{in}}{R_1}$ .

Since  $I_{amp} = 0$ ,  $I - I_{amp} = I$ ,  
 and  $V_{out} = I(R_1 + R_f)$   
 $= \frac{V_{in}}{R_1} (R_1 + R_f)$

$$\text{so } G = \frac{V_{out}}{V_{in}} = 1 + \frac{R_f}{R_1}$$

5.)



• Since  $I_{amp} = 0$  at input,  
 $V_+ = \frac{V_1}{2} R = \frac{V_1}{2}$

• since  $V_- = V_+$ ,  $V_- = \frac{V_1}{2}$

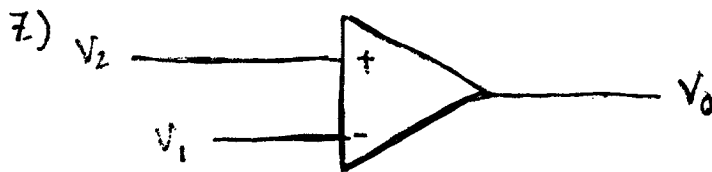
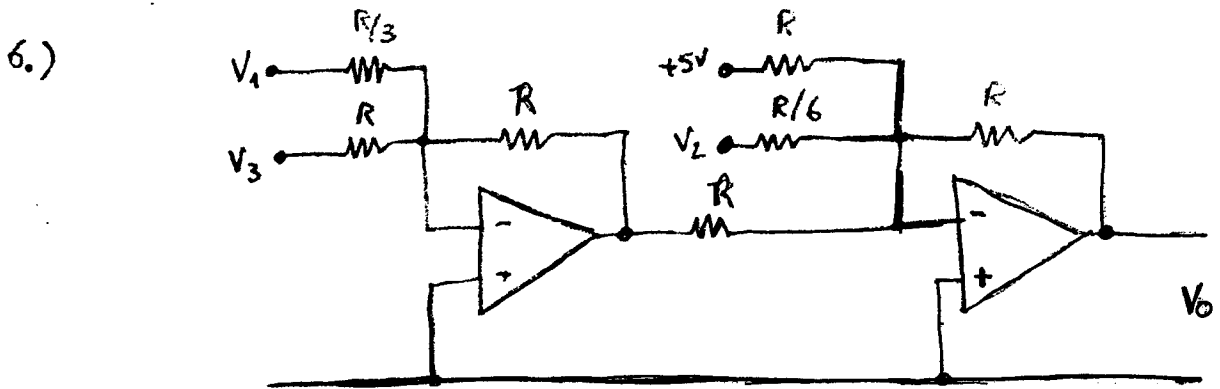
• thus  $I_2 = \frac{V_2 - V_-}{R} = \frac{V_2 - \frac{V_1}{2}}{R}$

• Since  $I_{amp} = 0$ ,  $I_2$  also is

$$I_2 = \frac{V_- - V_0}{R} = \frac{\frac{V_1}{2} - V_0}{R}$$

• thus  $\frac{\frac{V_1}{2} - V_0}{R} = \frac{V_2 - \frac{V_1}{2}}{R} \Rightarrow \boxed{V_0 = V_1 - V_2}$

Set #5, out



Since  $V_o = A(V_2 - V_1)$  only for  $|V_o| \leq$  limiting value set by the power supply (typically  $\pm 12V$ ),  $V_o$  will be at the limit when

$$V_2 - V_1 \geq \frac{V_L}{A} \quad \left( \sim \frac{12V}{10^6} = 12\mu V \right)$$

thus  $V_o = +V_L$  when  $V_2 > V_1 + \frac{V_L}{A}$ ,

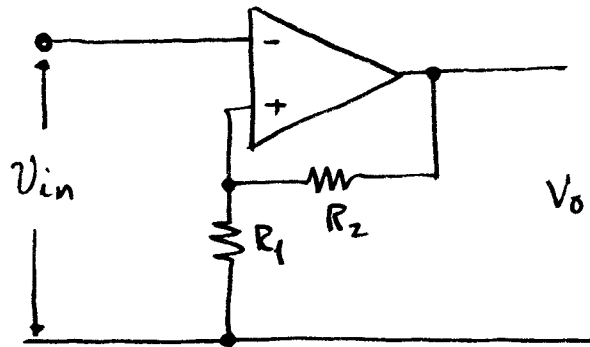
and  $V_o = -V_L$  when  $V_2 < V_1 - \frac{V_L}{A}$ .

Since  $\frac{V_L}{A} \approx 0$ ,  $V_o$  is the result of a comparison between

$V_2$  and  $V_1$ , e.g.,  $V_o = +V_L$  for  $V_2 > V_1$  +  $V_o = -V_L$  for  $V_2 < V_1$

Set 5, electronics

8.)

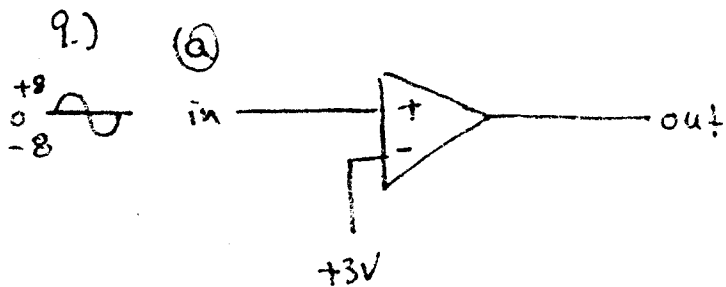


this is similar to the comparator, except that the voltage applied to the + input is derived from the output. Since the output will be either  $\pm V_L$  ( $V_L = V_{limit}$ ),

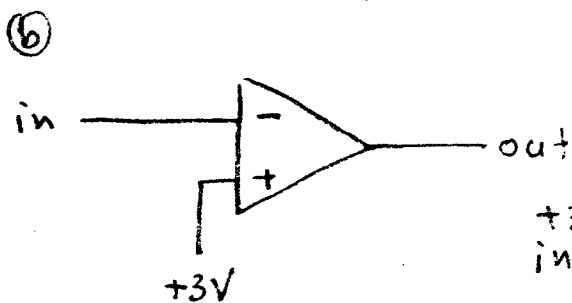
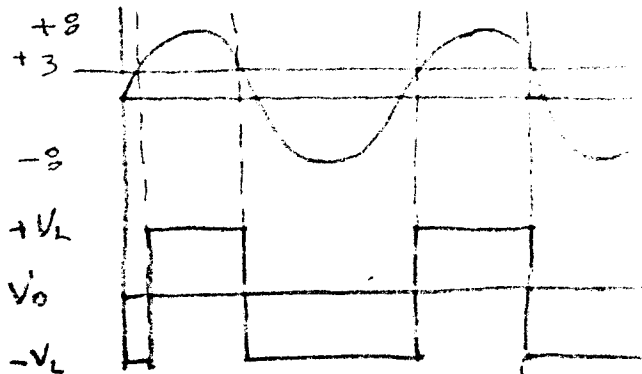
$$V_+ = \frac{\pm V_L}{(R_1 + R_2)} R_1.$$

the difference between this circuit and the one of # 7 is that  $V_{in}$  is compared to different voltages at each successive transition. Specifically, one time  $V_+$  is compared to, e.g.,  $+V_L \left( \frac{R_1}{R_1 + R_2} \right)$  until  $V_o$  makes the  $+V_L \rightarrow -V_L$  transition, and then  $V_i$  is compared to  $-V_L \left( \frac{R_1}{R_1 + R_2} \right)$ .

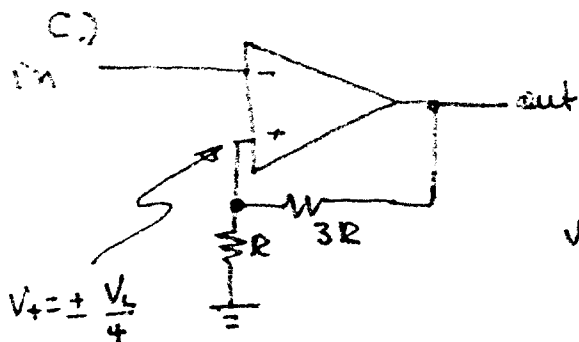
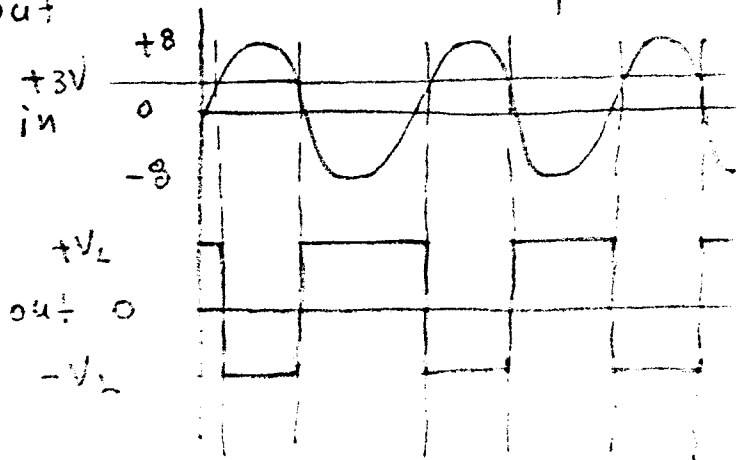
Electronics set #5, cont



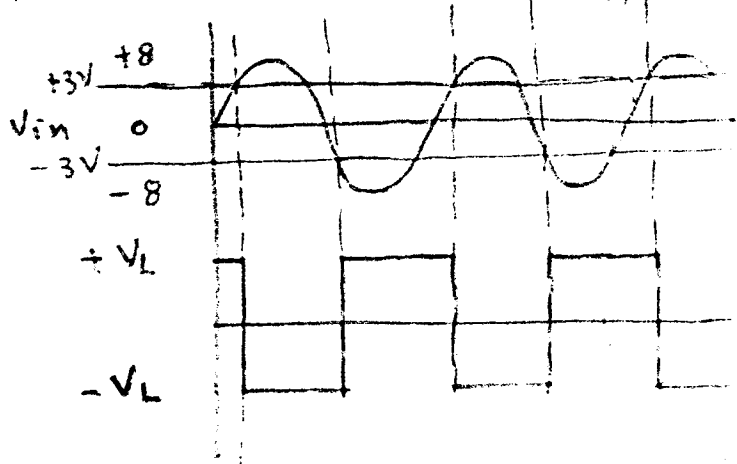
this is a comparator:



this is also a comparator:



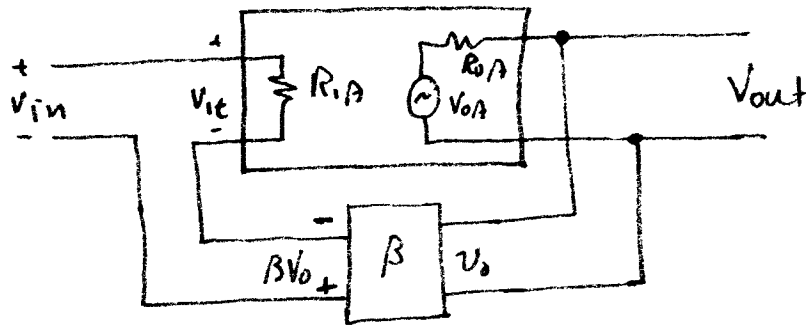
this is a Schmitt trigger



$V_+ = \pm \frac{V_L}{4}$   
 $V_L = 12V$  (given)  
 $V_T = \pm 3V$

# Homework Set #5, cont

10.)



a.) • by a loop analysis,

$$v_{in} = -\beta v_o + v_{it} \rightarrow v_{it} = v_{in} + \beta v_o$$

$$\bullet v_o = A v_{it} = A (v_{in} + \beta v_o)$$

$$\Rightarrow v_o (1 - A\beta) = A v_{in}$$

$$G = \frac{v_o}{v_{in}} = \frac{A}{1 - \beta A}$$

b.)  $R_{in} = \frac{v_{in}}{I_{in}} ; \text{ but } I_{in} = \frac{v_{it}}{R_{1A}}$

also,  $v_{it} = v_{in} + \beta v_o = v_{in} + \beta G v_{in} = v_{in} \left( \frac{1 - \beta A}{1 - \beta A} \right)$

so  $v_{it} = \frac{1}{1 - \beta A} v_{in}$

$$\therefore R_{in} = \frac{v_{in}}{I_{in}} = \frac{v_{in}}{v_{it}} R_{1A} = R_{1A} \frac{v_{in}}{v_{in} \left( \frac{1}{1 - \beta A} \right)} = \boxed{R_{in} (1 - \beta A)}$$

Electronics, H.W. 5, cont

10c) the relation given comes from Thevenin's theorem. Calculation of the numerator is basically as was done for (a): (negative feedback is assumed)

$$V_{LT} = \frac{V_o}{A} = V_{in} + \beta V_o \Rightarrow V_o|_{open} = V_{in} \frac{A}{1-\beta A}$$

↑  
this step assumes  $V_o = V_{oA}$ , or that no current flows in the output loop

The denominator requires the same procedure, but care in noticing the effect on things when the output is shorted.

$$I_{out}|_{short} = \frac{V_{oA}}{R_{oA}} = \frac{A V_{LT}}{R_{oA}}$$

note that  $V_{LT} = V_{in} + \beta V_o$ , but  $V_o = 0$  when the output is shorted. So

$$V_{LT}|_{out \text{ shorted}} = V_{in} + 0 = V_{in}$$

and

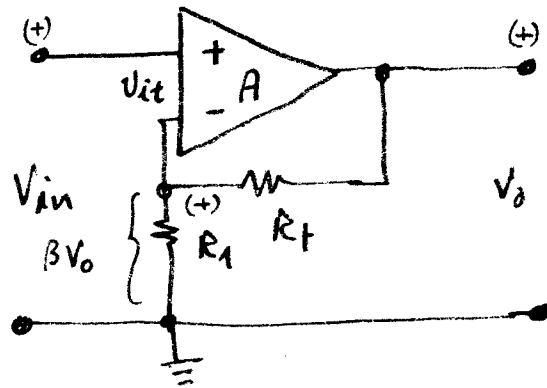
$$I_{out}|_{short} = \frac{A V_{LT}}{R_{oA}} = \frac{A V_{in}}{R_{oA}}$$

So

$$R_o = \frac{V_o|_{open}}{I_o|_{short}} = \frac{\left\{ V_{in} \frac{A}{1-\beta A} \right\}}{\left\{ \frac{A V_{in}}{R_{oA}} \right\}} = \frac{R_{oA}}{1-\beta A}$$

Homework Set #5, cont.

11.)



$$\bullet \quad BV_o = \left( \frac{R_1}{R_1 + R_f} \right) V_o \quad \Rightarrow \quad \beta = \frac{R_1}{R_1 + R_f}$$

$$\text{so. } V_{it} = V_{in} - \beta V_o; \quad V_o = AV_{it} = A(V_{in} - \beta V_o)$$

$$V_o = V_{in} \frac{A}{1 + A\beta}$$

$$\bullet \quad \boxed{\frac{V_o}{V_{in}} = \frac{A}{1 + A\beta} = \frac{A}{1 + A \left( \frac{R_1}{R_1 + R_f} \right)}}$$

$$\bullet \quad \lim_{A \rightarrow \infty} G = \lim_{A \rightarrow \infty} \frac{A}{1 + A\beta} = \lim_{A \rightarrow \infty} \frac{1}{1/\beta + A} = \frac{1}{\beta}$$

$$\text{Thus } \boxed{\lim_{A \rightarrow \infty} G = \frac{1}{\beta} = \frac{R_1 + R_f}{R_1} = 1 + \frac{R_f}{R_1}}$$